

Elastic models

Spring structure

Numerical solution of ODE

Cloth simulation

Numerical solution of ODE

General formulation

Consider relation given a system of **first order** differential equation

Mechanical systems are often expressed as

- *single equation of second order in p*

- *system of first order in $u = (p, v)$*

In general, we can write

$$u'(t) = \mathcal{F}(u(t), t)$$

If \mathcal{F} is an affine function in u

$$u'(t) = A(t) u(t) + b(t)$$

When A is constant through time

$$u'(t) = A u(t) + b(t)$$

Example: Free fall under gravity

- Force $F(t) = m g$

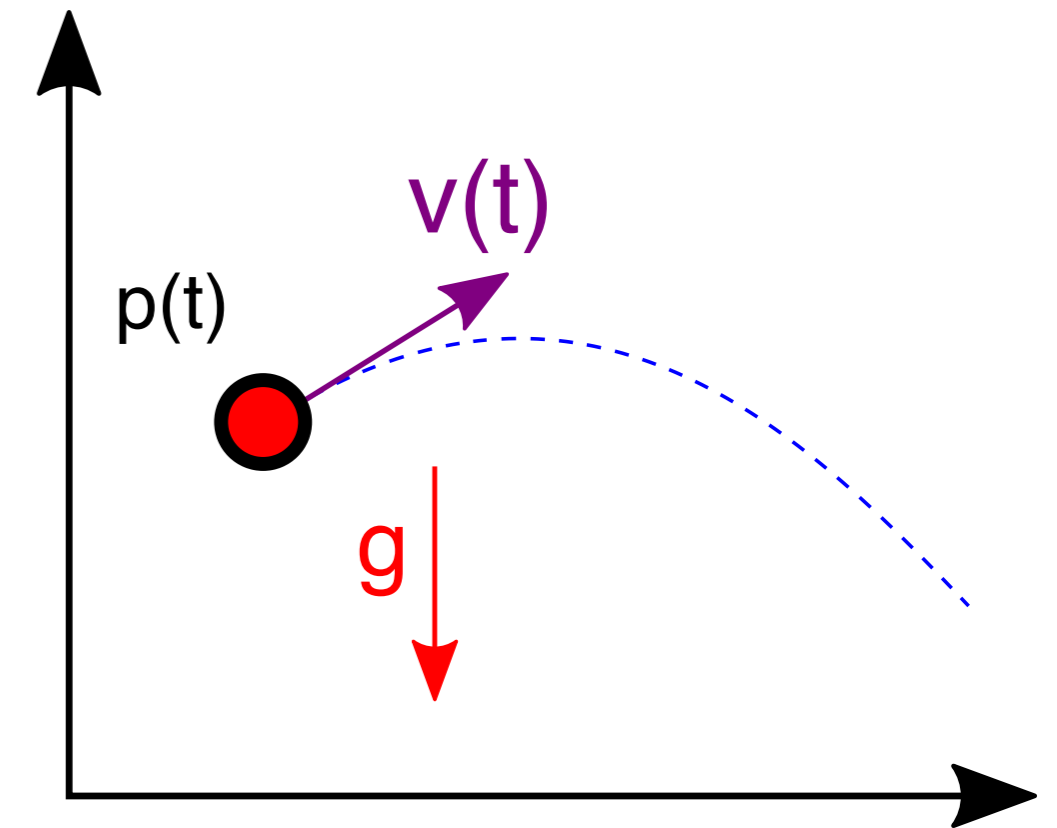
- Second order differential equation: $p''(t) = g$

- First order system $\underbrace{\begin{pmatrix} p \\ v \end{pmatrix}}_{u'(t)} (t) = \underbrace{\begin{pmatrix} v(t) \\ g \end{pmatrix}}_{\mathcal{F}(u,t)}$

- Linear system $\underbrace{\begin{pmatrix} p \\ v \end{pmatrix}}_{u'(t)} (t) = \underbrace{\begin{pmatrix} 0 & 1 \\ 0 & 0 \end{pmatrix}}_A \underbrace{\begin{pmatrix} p \\ v \end{pmatrix}}_{u(t)} (t) + \underbrace{\begin{pmatrix} 0 \\ g \end{pmatrix}}_{b(t)}$

- Exact solution known: $p(t) = \frac{1}{2} g t^2 + v_0 t + p_0$

Note: variables are vectors - matrix can be expressed by block, or per components.



Example: 1D spring (/ Harmonic oscillator)

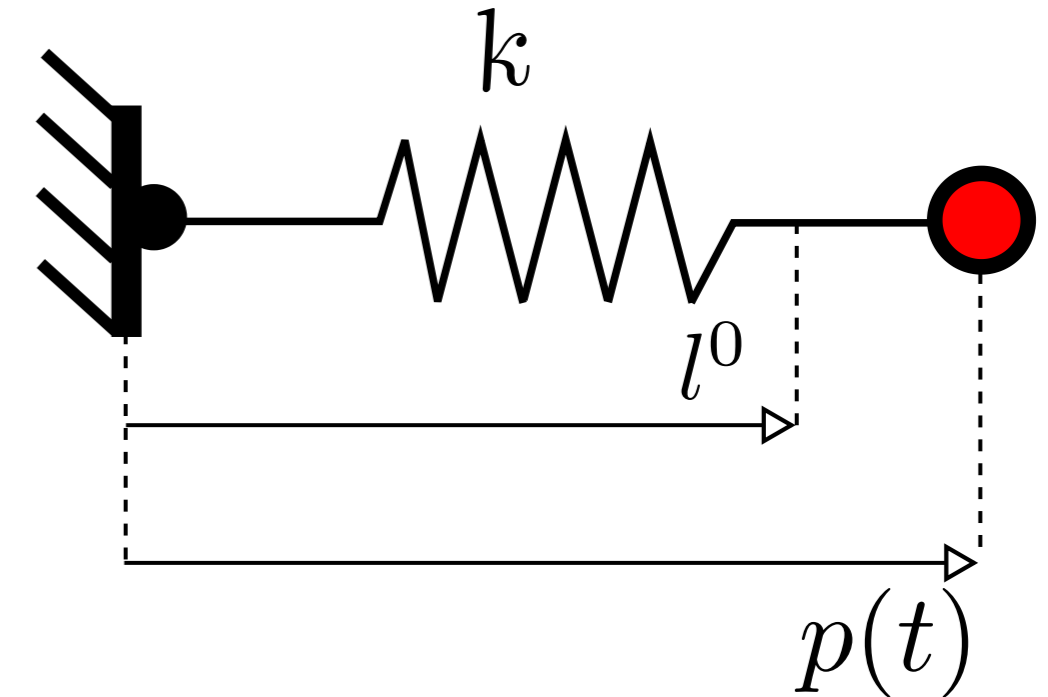
- Force $F(t) = -k(p(t) - l^0)$, k spring stiffness, l^0 rest length
- Second order differential equation: $m p''(t) + k p(t) = k l^0$

- First order system
$$\underbrace{\begin{pmatrix} p \\ v \end{pmatrix}}_{u'(t)}'(t) = \underbrace{\begin{pmatrix} v(t) \\ -k/m(p(t) - l^0) \end{pmatrix}}_{\mathcal{F}(u,t)}$$

- Linear system
$$\underbrace{\begin{pmatrix} p \\ v \end{pmatrix}}_{u'(t)}'(t) = \underbrace{\begin{pmatrix} 0 & 1 \\ -k/m & 0 \end{pmatrix}}_A \underbrace{\begin{pmatrix} p \\ v \end{pmatrix}}_{u(t)}(t) + \underbrace{\begin{pmatrix} 0 \\ k/m l^0 \end{pmatrix}}_b$$

- Exact solution known: $p(t) = A \sin(\omega t + \varphi) + l^0$

$$\omega = \sqrt{k/m}, A^2 = (p^0 - l^0)^2 + \left(\frac{v_0}{\omega}\right)^2, \tan(\varphi) = \frac{p^0 - l^0}{v_0/\omega}$$

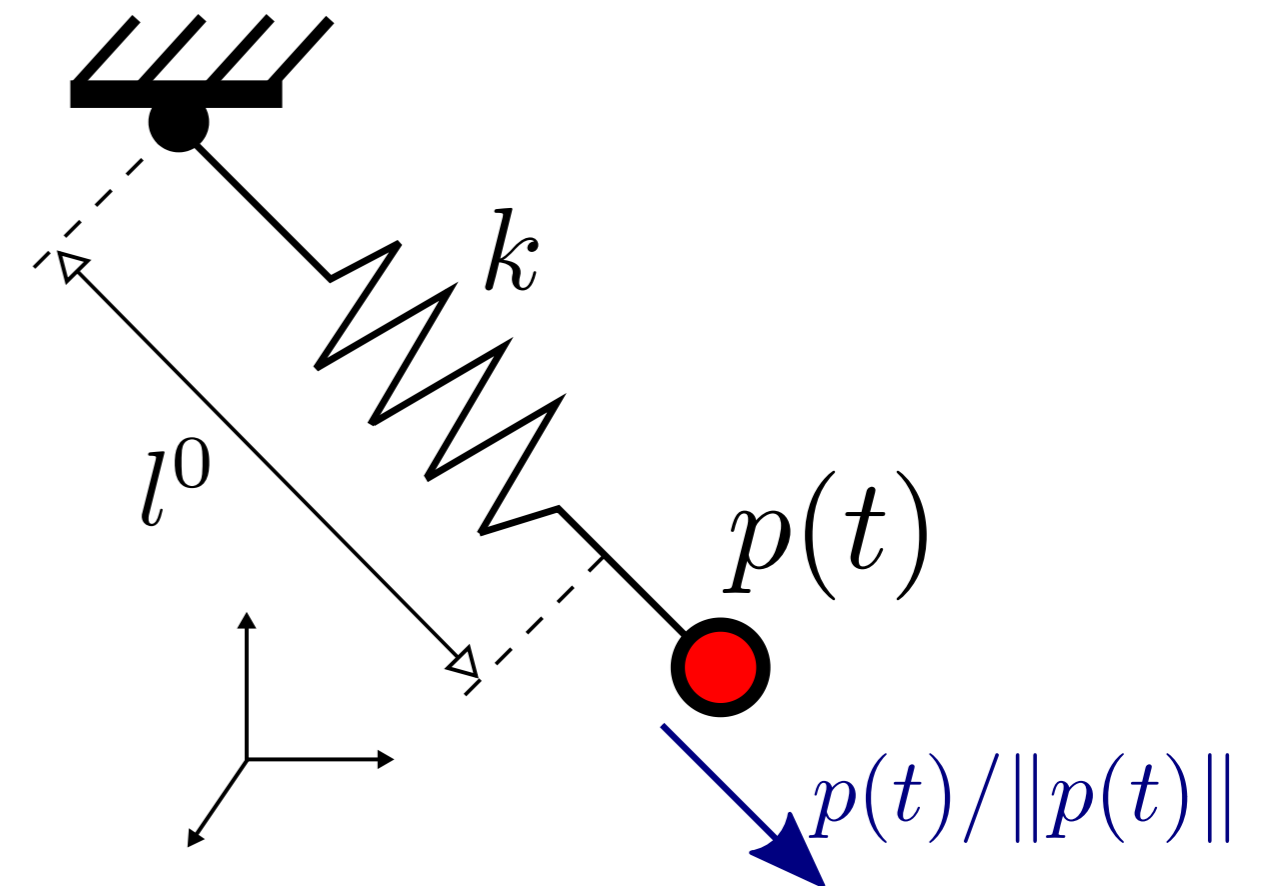


Example: 3D mass spring

- Force $F(t) = m g - k (\|p(t)\| - l^0) \frac{p(t)}{\|p(t)\|}$, k spring stiffness, l^0 rest length
- Second order differential equation: $m p''(t) = m g - k (\|p(t)\| - l^0) \frac{p(t)}{\|p(t)\|}$

- First order system $\underbrace{\begin{pmatrix} p \\ v \end{pmatrix}}_{u'(t)} (t) = \underbrace{\begin{pmatrix} v(t) \\ g - k/m (\|p(t)\| - l^0) \frac{p(t)}{\|p(t)\|} \end{pmatrix}}_{\mathcal{F}(u,t)}$

- Not linear
- No simple explicit solution



Numerical solution

1st order Explicit Euler

Naive numerical scheme: Approximation of the derivative

$$\frac{u^{k+1} - u^k}{h} = \mathcal{F}(u^k, t^k)$$

$$\Rightarrow u^{k+1} = u^k + h \mathcal{F}(u^k, t^k)$$

In the linear case

$$u^{k+1} = (\mathbf{I} + h \mathbf{A}) u^k + h b^k$$

Pro : very easy to implement

Is u^k a good approximation of the true solution $\tilde{u}(t^k)$?

For a single particle with p, v variables:

$$\begin{cases} v^{k+1} = v^k + h F(u^k, t^k)/m \\ p^{k+1} = p^k + h v^k \end{cases}$$

Explicit Euler - study case

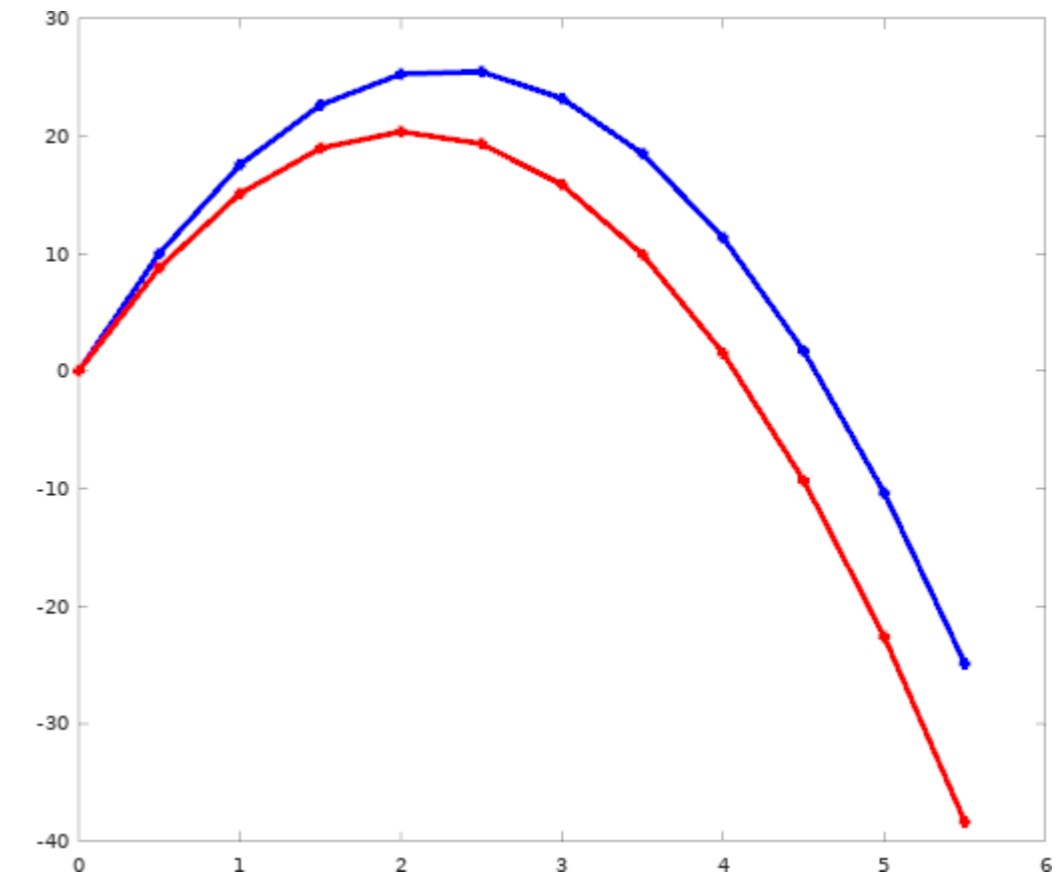
Free fall under gravity

- True solution $\tilde{u}(k h) = p_0 + (k h)v_0 + \frac{(k h)^2}{2} g$

- Numerical scheme: $\begin{pmatrix} p \\ v \end{pmatrix}^{k+1} = \begin{pmatrix} 1 & h \\ 0 & 1 \end{pmatrix} \begin{pmatrix} p \\ v \end{pmatrix}^k + \begin{pmatrix} 0 \\ h g \end{pmatrix}$

- Numerical solution: $p^k = p_0 + k h v_0 + \frac{k(k-1)}{2} h^2 g$

\Rightarrow **Not exact** : Error $e^k = |u^k - \tilde{u}(k h)| = \frac{g}{2} k h^2$



red: true solution

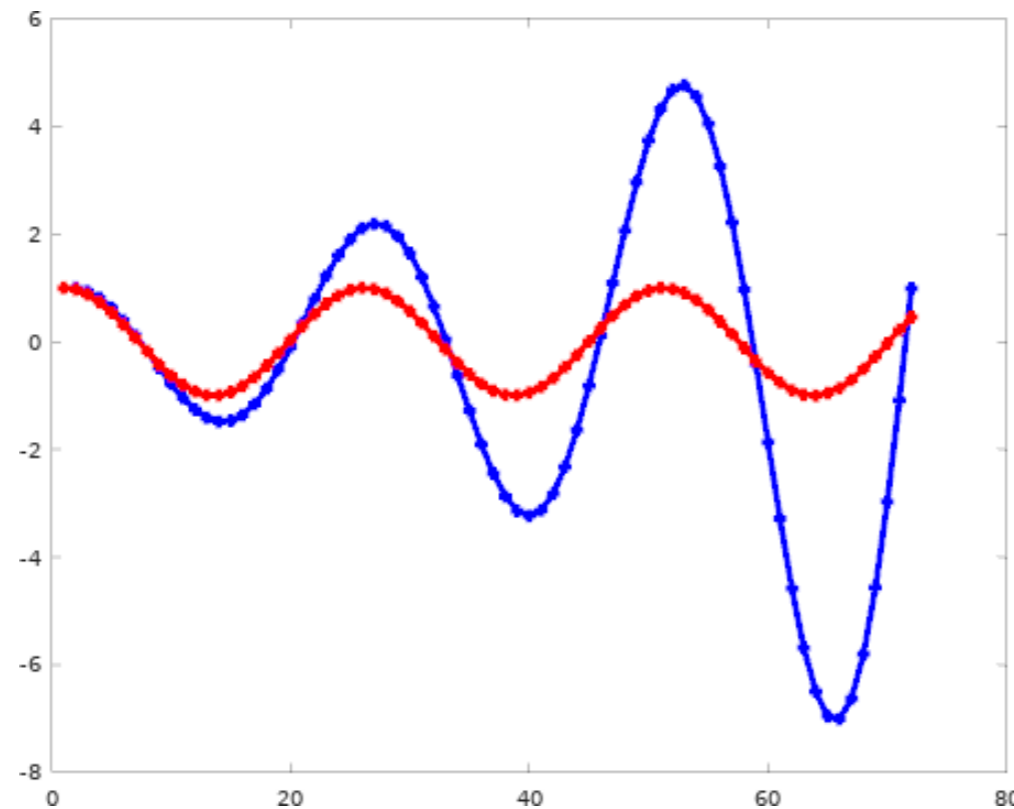
blue: numerical solution

Explicit Euler - study case

1D spring

- True solution: permanent oscillation

- Numerical scheme:
$$\begin{pmatrix} p \\ v \end{pmatrix}^{k+1} = \begin{pmatrix} 1 & h \\ -K/m h & 1 \end{pmatrix} \begin{pmatrix} p \\ v \end{pmatrix}^k + \begin{pmatrix} 0 \\ K/m h t^0 \end{pmatrix}$$



red: true solution

red: numerical solution

- Numerical solution diverge to ∞
- Worse than bad accuracy for Graphics

Explicit Euler - study case

1D spring: Analysis of the system energy

- Energy $E = \frac{1}{2}mv^2 + \frac{K}{2}(p - l^0)^2$

$$E^{k+1} = \frac{1}{2}m \left(-\frac{K}{m}\Delta t (p^k - l^0) + v^k \right)^2 + \frac{1}{2}K (p^k + \Delta t v^k - l^0)^2$$

$$E^{k+1} = \underbrace{\frac{1}{2}m (v^k)^2 + \frac{1}{2}K (p^k - l^0)^2}_{E^k} + \frac{1}{2} \left[\underbrace{\frac{K^2}{m} (\Delta t)^2 (p^k - l^0)^2}_{>0} - \underbrace{2K\Delta t (p^k - l^0) v^k}_{=0} + \underbrace{2K\Delta t (p^k - l^0) v^k}_{=0} + \underbrace{K(\Delta t)^2 (v^k)^2}_{>0} \right]$$

$$E^{k+1} = E^k + \epsilon (\Delta t)^2, \epsilon > 0$$

⇒ gain of energy

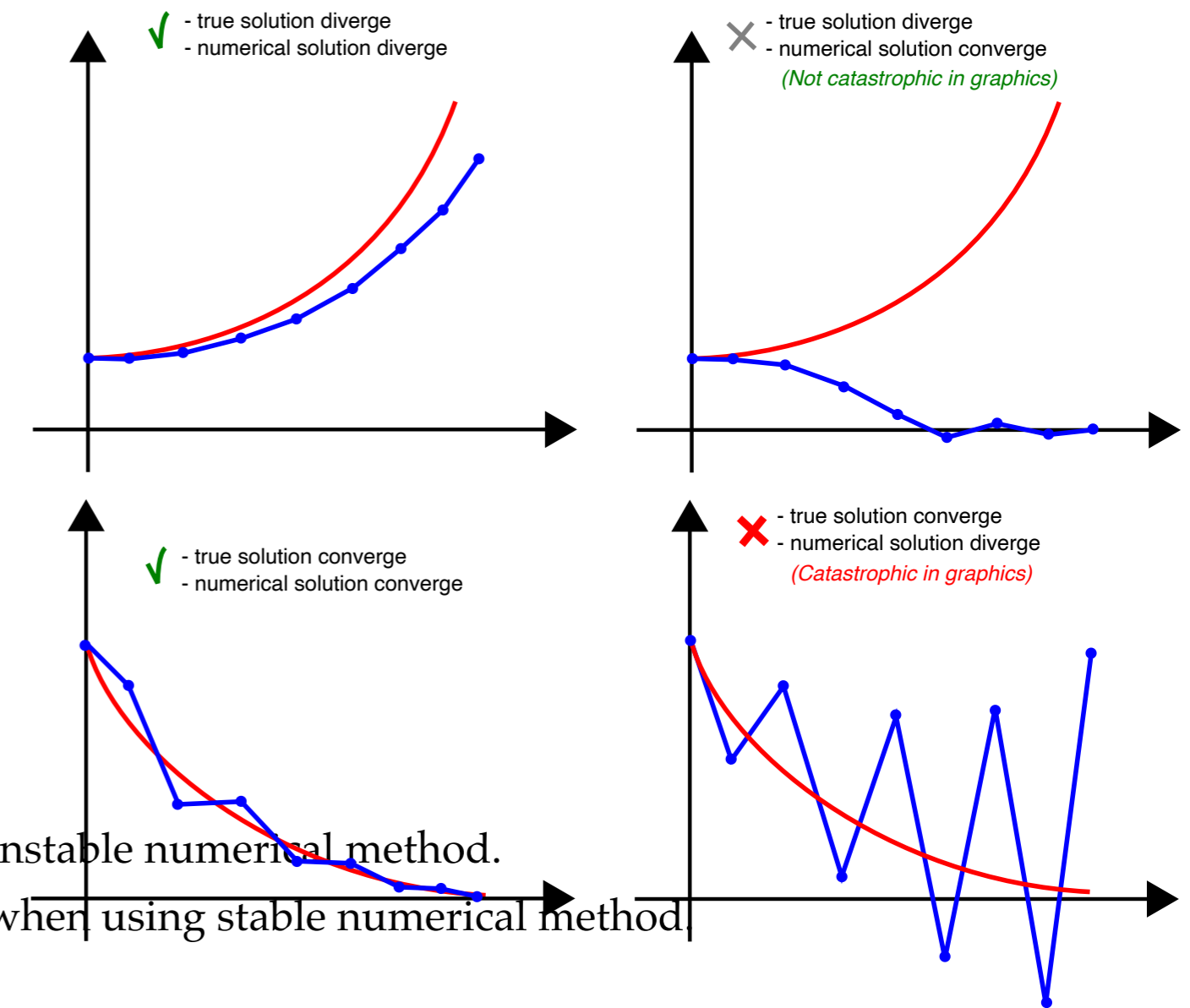
⇒ divergence

Stability of a numerical method - general definition

- Classical stability of a method studied on $u'(t) = \lambda u(t)$, $\lambda \in \mathbb{C}$.
 - The true solution $\tilde{u}(t) = \exp(\lambda t)$ converge if $\Re_e(\lambda) \leq 0$.
 - For linear system, λ refers to eigenvalues of A.
 - For non linear system, λ refers to eigenvalues of the Jacobian of \mathcal{F}
- A numerical method is *unconditionnaly stable* if $\Re_e(\lambda) \leq 0 \Rightarrow$ stable discrete solution.
- Otherwise, it is conditionnaly stable / unstable.
- Region of stability:
Set of conditions on λ such that the discrete solution doesn't diverge.

Rem.

- A numerical solution can diverge even when the true ODE solution converge when using unstable numerical method.
- Converseley, a numerical solution can converge even when the true ODE solution diverge when using stable numerical method.
- Stability ! = Accuracy.



Stability analysis of explicit Euler

$$u'(t) = \lambda u(t)$$

$$\Rightarrow u^{k+1} = u^k + \lambda u^k \text{ using explicit Euler}$$

$$\Rightarrow u^{k+1} = (1 + \lambda h) u^k$$

$$\Rightarrow \text{Stable if } |1 + \lambda h| \leq 1 \text{ (conditionnal stability)}$$

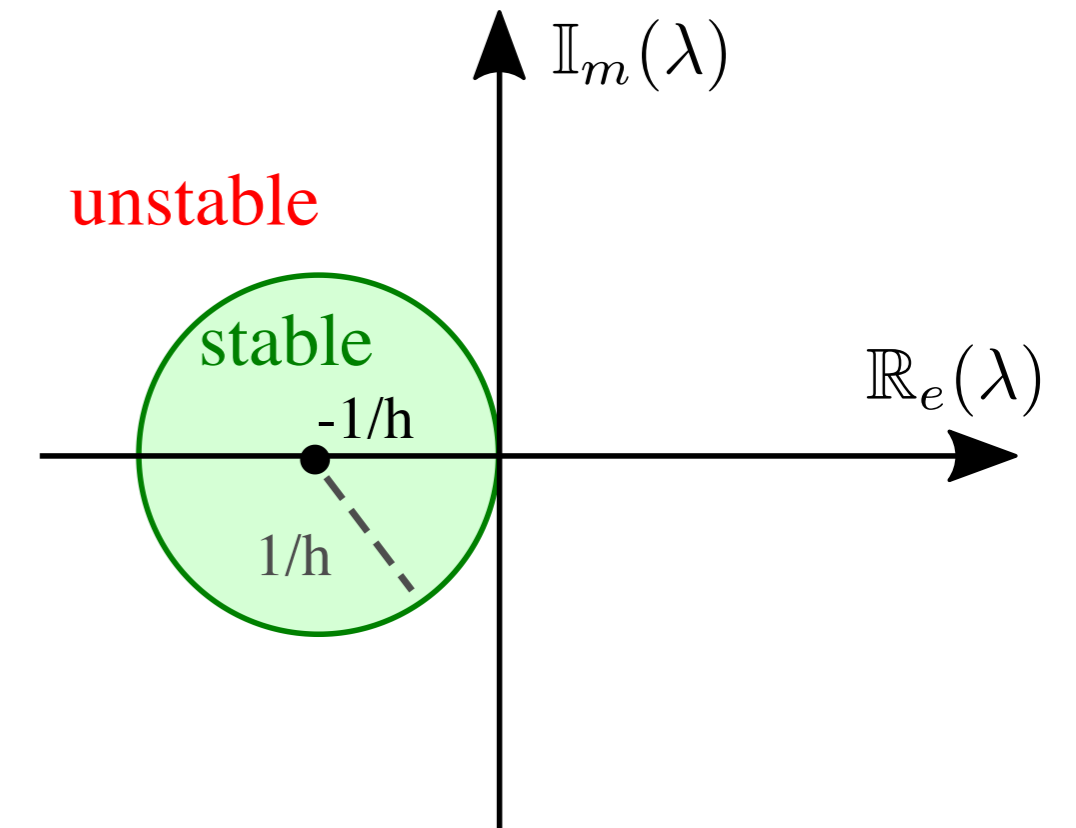
$$|1/h + \lambda| \leq 1/h: \text{ Interior of a disc centered on } (-1/h, 0) \text{ with radius } 1/h$$

Rem. For 1D elastic spring

$$\lambda = \pm i \sqrt{K/m}$$

$$\Rightarrow |1 + i \sqrt{K/m} h| = \sqrt{1 + K/m h^2} > 1$$

\Rightarrow Explicit euler is always unstable on the elastic spring problem.



Numerical integration of ODE

General formulation: $u'(t) = \mathcal{F}(u, t)$, $u(t) = (p(t), v(t))$.

Explicit Euler

$$u^{k+1} = u^k + \Delta t \mathcal{F}(u^k, t^k)$$

(+) Easy to implement

(-) Worst scheme in all cases (divergence, low accuracy)

Explicit Runge-Kutta

$$u^{k+1} = u^k + \Delta t \sum_j \alpha_j k_j$$

(+) Good **accuracy**

(+) Efficient to apply

(+/-) Stability OK for non-stiff problem, diverge on stiff problem

(-) Artificial damping for constant energy system

Implicit methods

$$u^{k+1} = u^k + \Delta t \mathcal{F}(u^{k+1}, t^{k+1})$$

(+) Good to deal with **stiff problem** - very stable

(-) Add numerical damping (converge even if solution oscillates)

(-) Hard / computationally costly to apply on non linear problem

Symplectic integrator

$$v^{k+1} = v^k + \Delta t F^k / m$$

$$p^{k+1} = p^k + \Delta t v^{k+1}$$

(+) Handle well constant energy system, preserves energy (Hamiltonian systems)

(+) Simple and efficient to implement

(-) Less accurate than RK

(-) Diverge on stiff problem

Introduction to symplectic methods

Standard approaches trade-off

- Explicit methods: (+) Simple to compute, (-) limited stability
- Implicit methods: (-) Hard to compute (especially on non linear functions), (+) very stable
- Oscillatory systems are not easy to model
 - (-) Numerical solution either diverge or converge.

Symplectic approach

- *Remark:* Mechanical systems have position and velocity variables
 - Derivative of position is linear w / r velocity
 - Derivative of velocity is more complex (forces - non linear)
- ⇒ *General idea:* separate treatment of velocity and position

Semi-implicit:

- Implicit scheme for position p^{k+1} (linear part)
 - Explicit scheme for velocity v^{k+1} (non linear part)
- ⇒ In practice: use velocity v^{k+1} to evaluate p^{k+1} .

Pro

- (+) As simple as explicit method to implement
- (+) Improved stability
- (+) Well adapted to oscillatory systems

Semi implicit method

Simplest semi-implicit method: **Semi-implicit Euler / Verlet**

General case

$$v^{k+1} = v^k + h \mathcal{F}_v(p^k, v^k, t^k)$$

$$p^{k+1} = p^k + h \mathcal{F}_p(p^k, v^{k+1}, t^k)$$

Application to classical mechanical cases

$$p'(t) = v(t), m v'(t) = F(p, t)$$

$$\Rightarrow \begin{cases} v^{k+1} = v^k + h F(p^k, t^k)/m \\ p^{k+1} = p^k + h v^{k+1} \end{cases}$$

(+) *Trivially easy to convert explicit Euler to semi-implicit Euler*

Expressed using positions only

$$p^{k+1} = p^k + h(v^k + h F(p^k, t^k))$$

$$p^{k+1} = p^k + h \left(\frac{p^k - p^{k-1}}{h} + h F(p^k, t^k)/m \right)$$

$$\Rightarrow p^{k+1} = 2p^k - p^{k-1} + h^2 F(p, t)/m$$

1st order accurate (like explicit/implicit Euler) in position and speed.

Stability on oscillatory system

1D spring system: $F(p^k, v^k, t^k) = -K p^k$

$$p^{k+1} = 2p^k - p^{k-1} - h^2 K/m p^k$$

$$\Rightarrow p^{k+1} = (2 - h^2 K/m) p^k - p^{k-1}$$

Stable and permanent oscillation when $h < \frac{2}{\sqrt{K/m}} = \frac{2}{\omega}$

Q. How can we demonstrate it ?

Note: $h < 2/\omega$ only valid for one 1D spring. Coupled 3D springs may require smaller value of h.

Use of semi-implicit

Ex. Elastic Spring: $F(p) = -K(p - L_0)$

Explicit Euler

```
for(int k=0; k<N; ++k) {  
    p = p + h*v;  
    v = v + h * F/m;  
}
```

(-) Always diverges for elastic problem

Semi-Implicit Euler

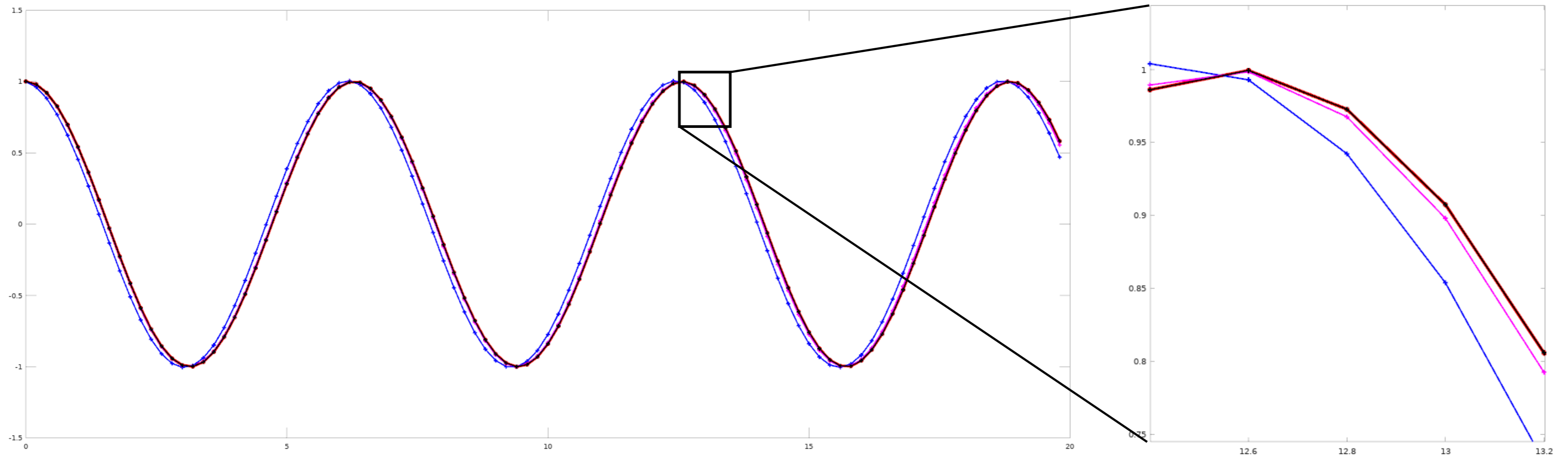
```
for(int k=0; k<N; ++k) {  
    v = v + h * F/m;  
    p = p + h*v;  
}
```

(+) Permanent oscillation for sufficiently small h .

⇒ Extremely simple change !
Big gain in stability

Comparison between approaches

Small $h = 0.2/\omega$

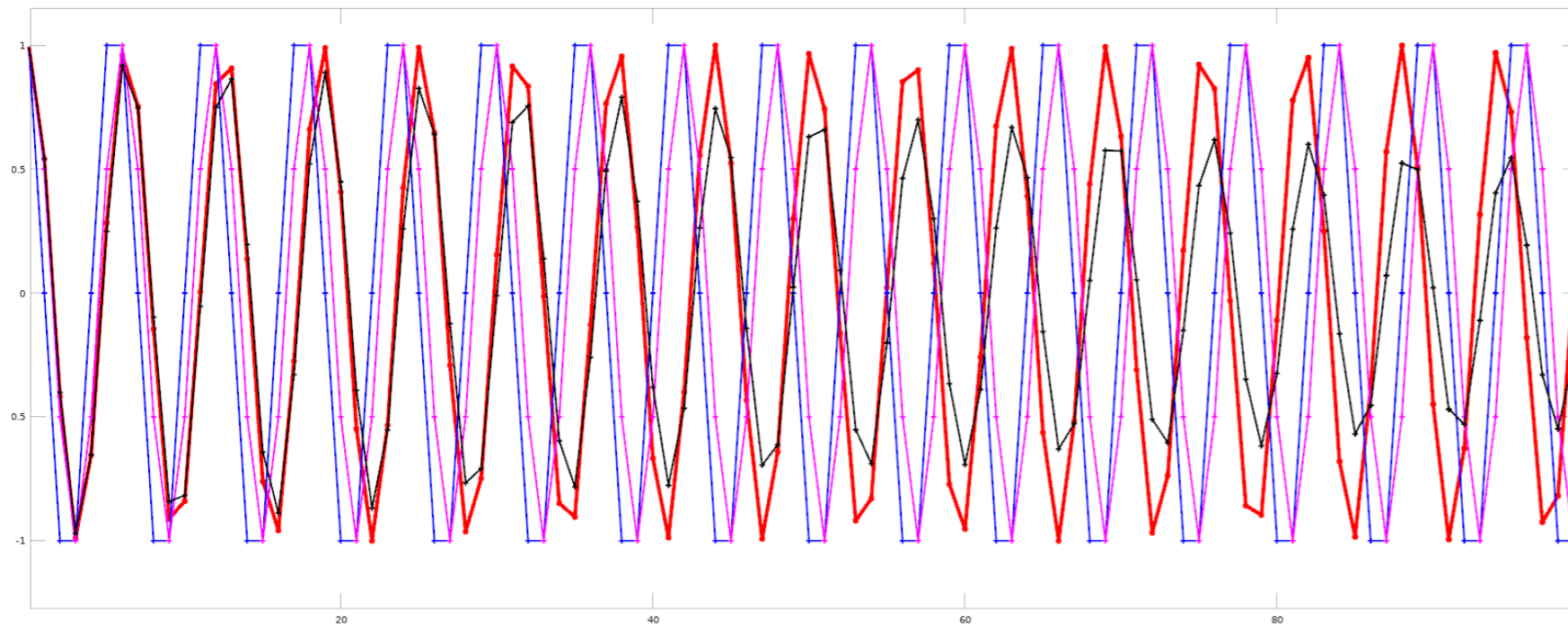


True solution , *Semi-implicit Euler* , *Velocity Verlet* , *Runge-Kutta RK4*

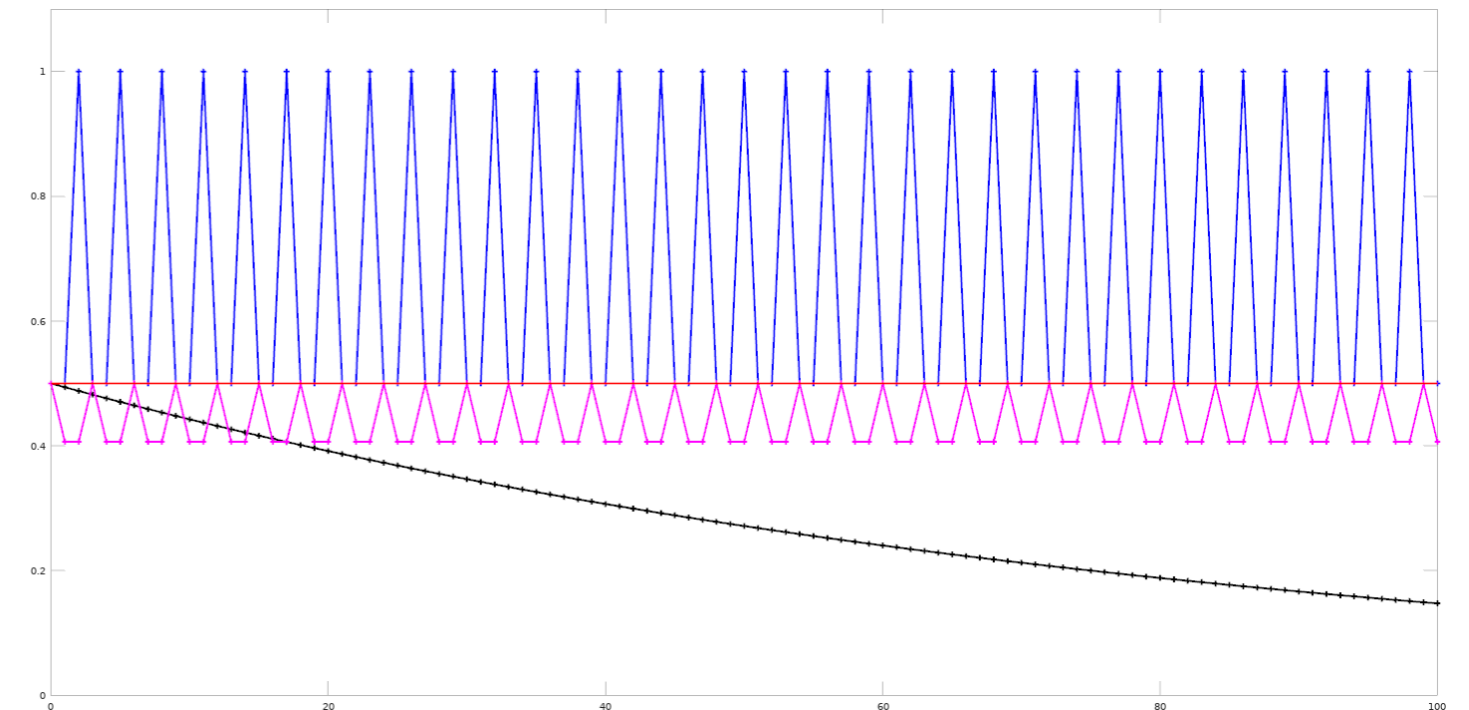
- RK4 - best behavior (undistinguishable from true solution)

Comparison between approaches

Larger $h = 1.0/\omega$



Temporal evolution of p^k



Temporal evolution of energy $E = 1/2m (v^k)^2 + 1/2K (p^k)^2$

True solution , *Semi-implicit Euler* , *Velocity Verlet* , *Runge-Kutta RK4*

- RK4 loose energy and p^k converge toward l^0
- Symplectic integrator keep oscillating

Material model

Elasticity: Shape goes back toward its original rest position when external forces are removed.

-Purely elastic models don't lose energy when deformed (potential \leftrightarrow kinetic)

Plasticity: Opposite of elasticity. Plastic material don't come back to their original shape (/ change their rest position during deformation).

- Ductile material - can allow large amount of plastic deformation without breaking (plastic)

- Brittle - Opposite (glass, ceramics)

Viscosity: Resistance to flow (usually for fluid, ex. honey)

In reality

- *Elasto-plastic materials:* Allow elastic behavior for small deformation, and plastic at larger one.

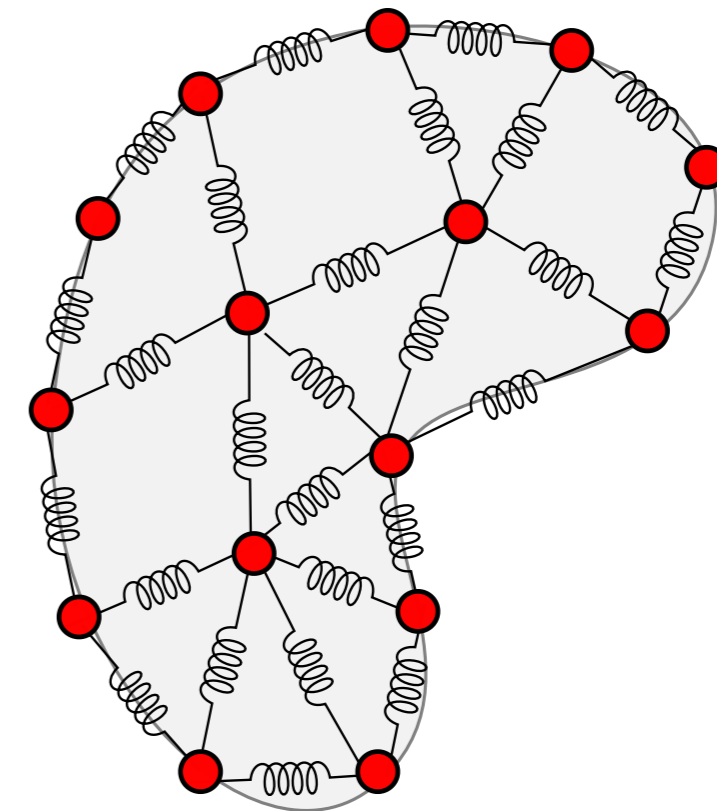
- *Visco-elastic materials:* Elastic properties with delay.



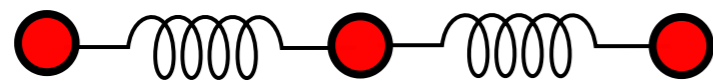
Modeling elastic shapes with particles

Spring mass systems

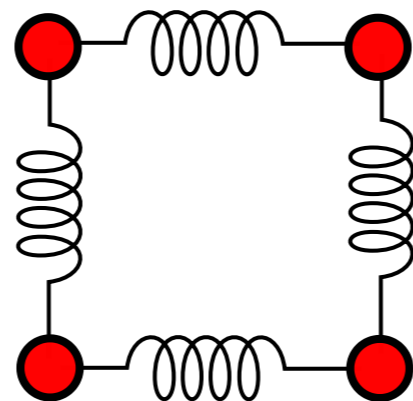
- Particles (position, velocity, mass): samples on shape
- Springs : link closed-by particles in the reference shape



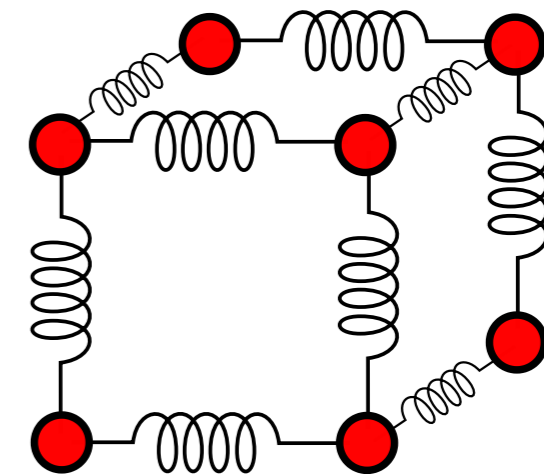
1D curve structure



2D surface structure



3D volume structure

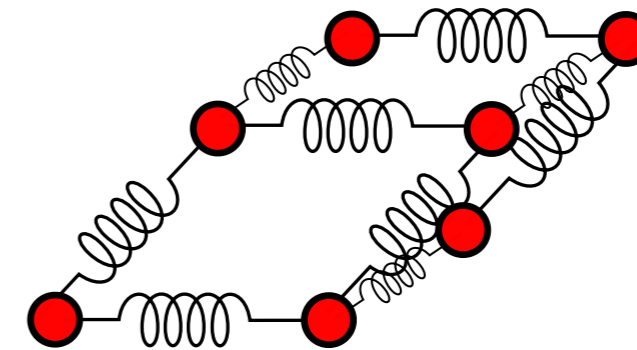
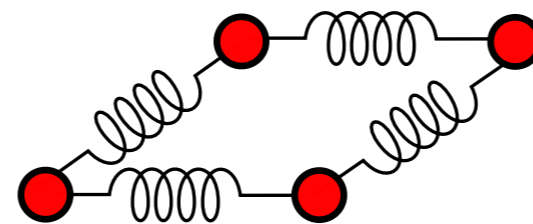
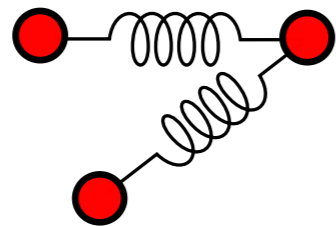


Spring structure

How to model spring connectivity ?

- **Structural springs:** 1-ring neighbors springs (\simeq mesh edges)

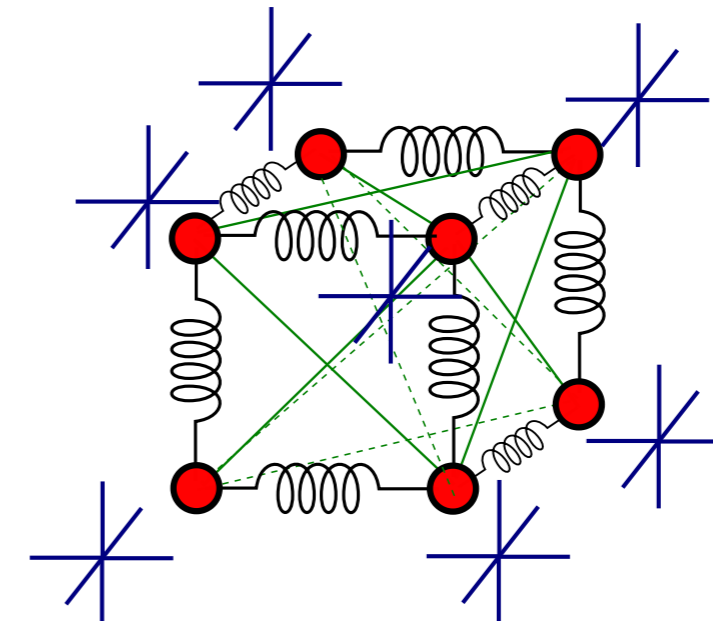
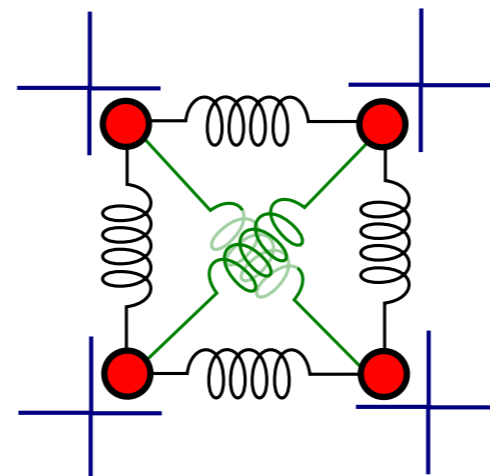
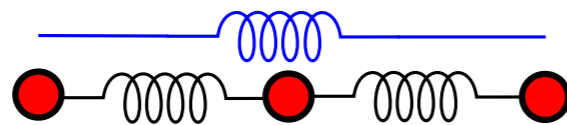
(+) Limit elongation/contraction, (-) Allows shearing, and bending



\Rightarrow Add extra springs connectivity

- **Shearing springs:** Diagonal links

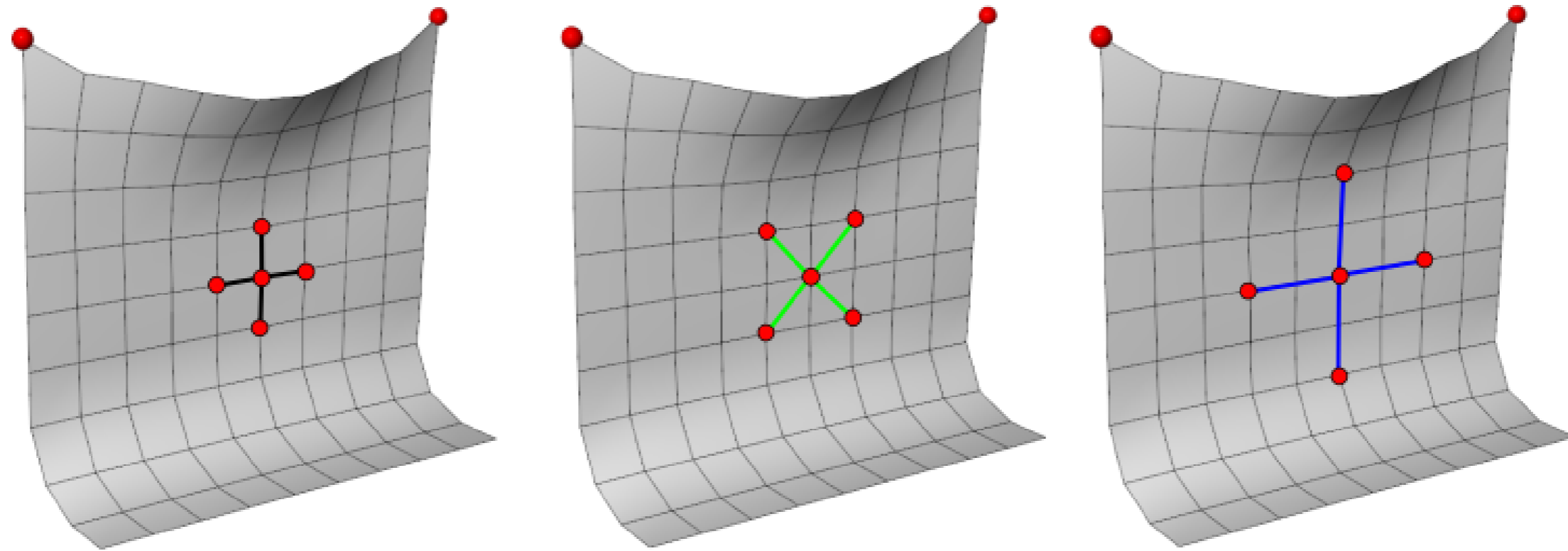
- **Bending springs:** 2-ring neighborhood



Cloth Simulation

Mass-spring cloth simulation

- Particles are sampled on a $N \times N$ grid.
 - Each particle has a mass m ($m_{cloth} = N^2 m$)
- Set structural, shearing and bending springs.



Forces

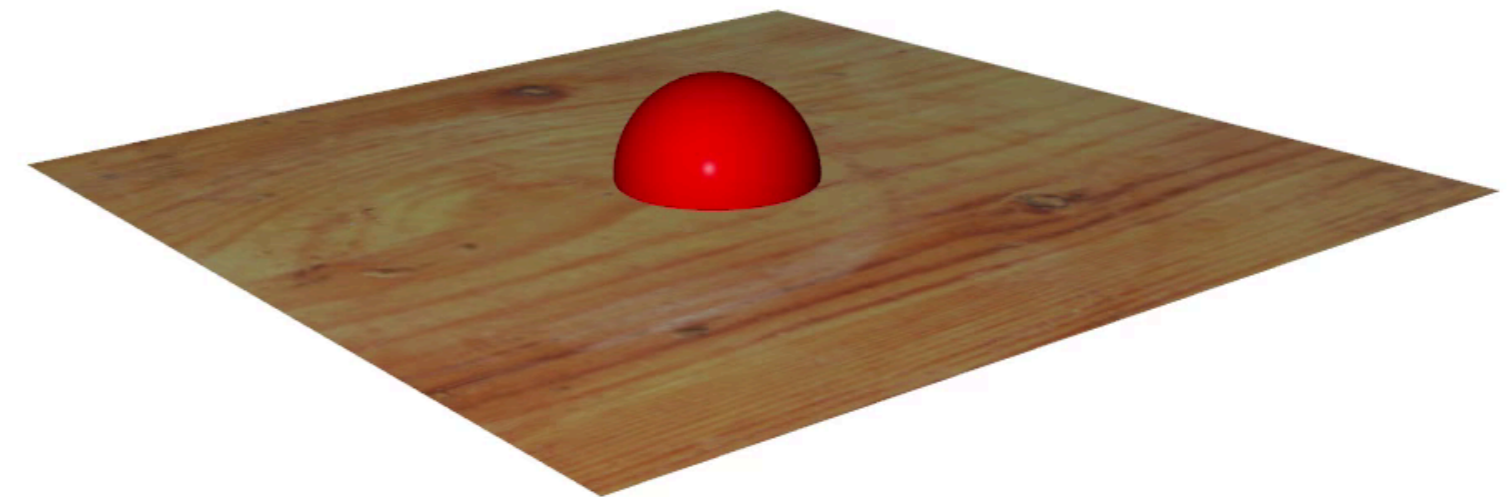
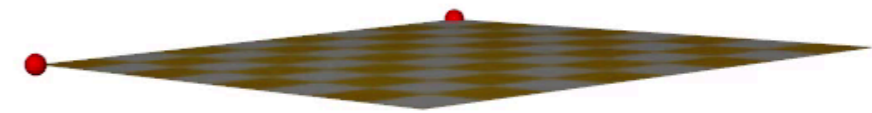
- On each particle: gravity + drag + spring forces

$$- F_i(p, v, t) = m_i g - \mu v_i(t) + \sum_{j \in \mathcal{V}_i} K_{ij} (\|p_j(t) - p_i(t)\| - L_{ij}^0) \frac{p_j(t) - p_i(t)}{\|p_j(t) - p_i(t)\|}$$

- \mathcal{V}_i : neighborhood of particle i

- L_{ij}^0 : rest length of spring ij

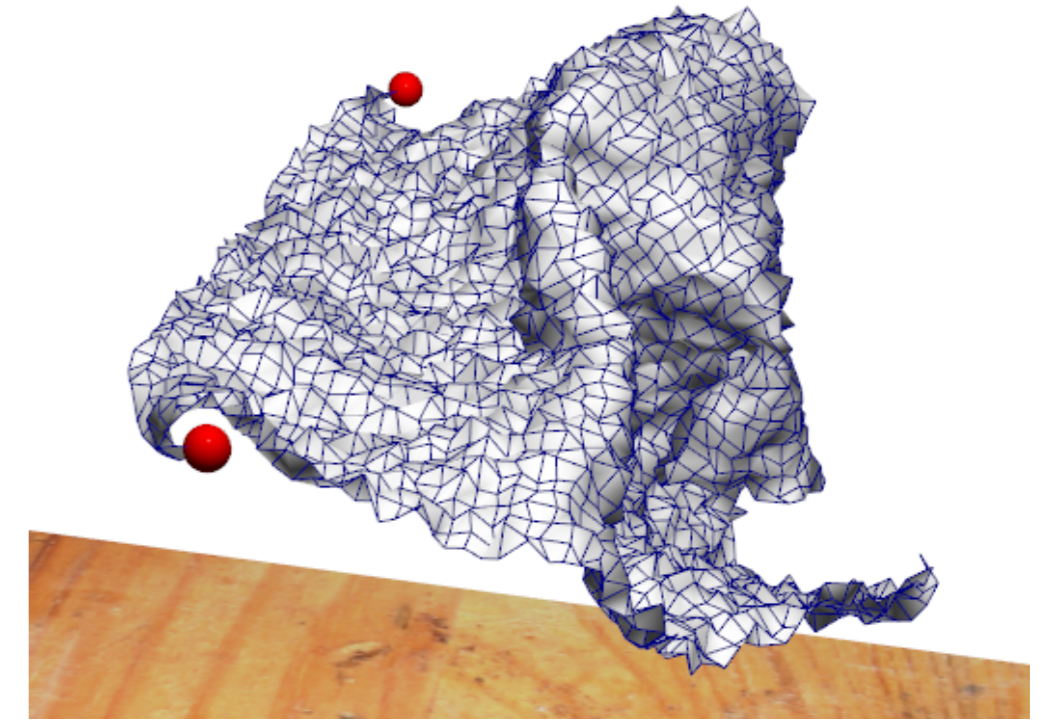
$$\text{Associated ODE } \forall i, \begin{cases} p_i'(t) = v_i(t) \\ v_i'(t) = F_i(p, v, t)/m_i \end{cases}$$



Q. How can we model the effect of the wind ?

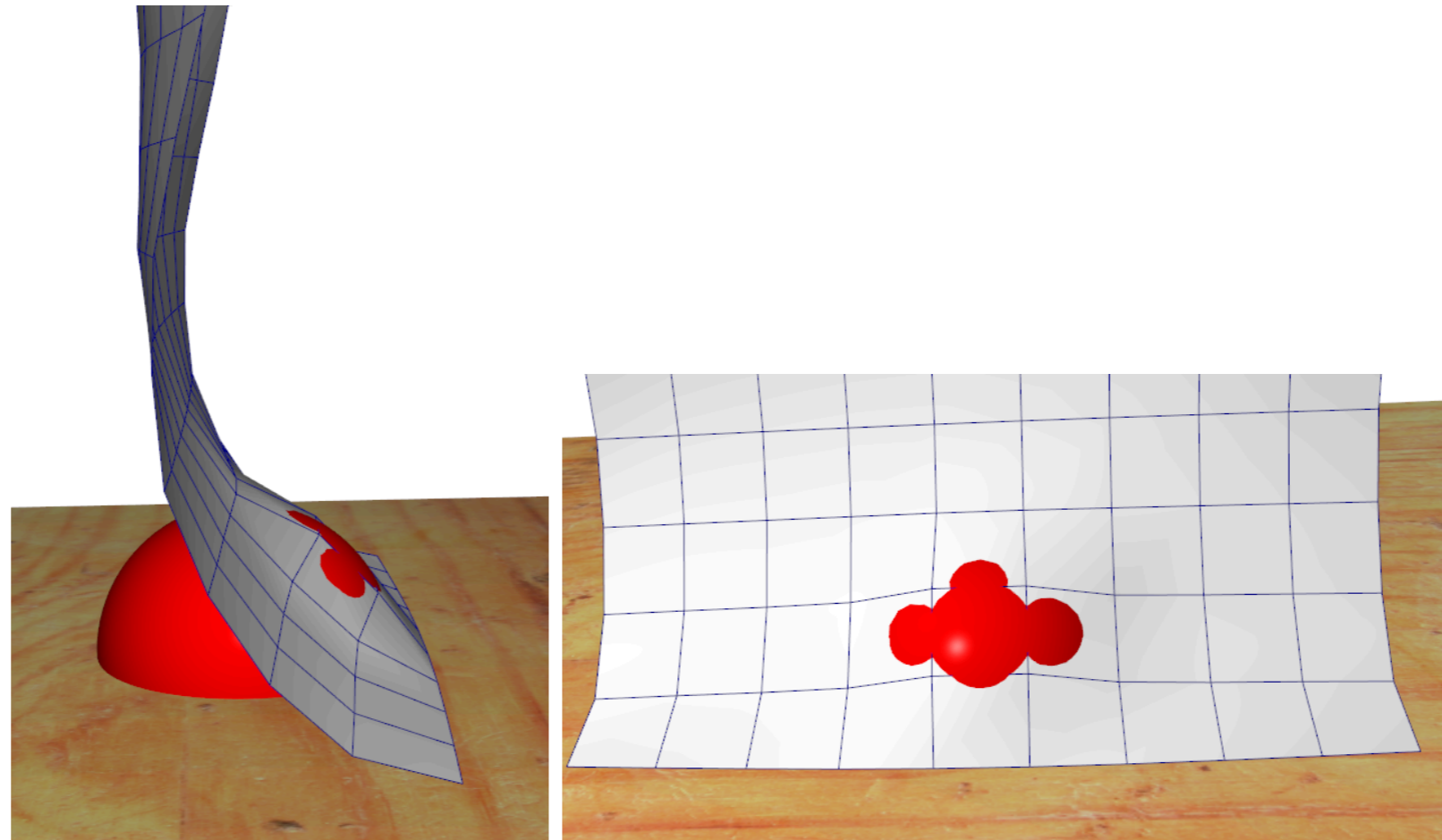
Note on Mass-Spring numerical solution

- Non-linear ODE
- Large K_{ij} : good length preservation, but stiff ODE
⇒ divergence of explicit schemes.
- Avoid explicit Euler (divergence)
- Semi-implicit Euler / Verlet works fine for low K_{ij}
Semi-implicit Euler + PBD allows simple integration + stable stiff springs
[Muller et al. [PBD](#) , [Inextensible clothing in Computer Games](#)]
- RK4 more accurate (but higher complexity than Verlet)
- Implicit Euler : requires linearization, but very stable



Collisions

- Simple approach : Handled as collision between particles and shapes
 - (+) Simple and efficient
 - (-) Collision may still appear within a triangle
- ⇒ Simplest solution: take an ϵ -margin around each collider.
Or Exhaustive approach: edges + faces (more costly).



Detecting self collision

Handled as moving point in collision with moving triangle

Inputs

- Triangle $P_1(t)P_2(t)P_3(t)$, a point $P(t)$
- Each position $P_k(t) = P_k(0) + t v_{P_k}$

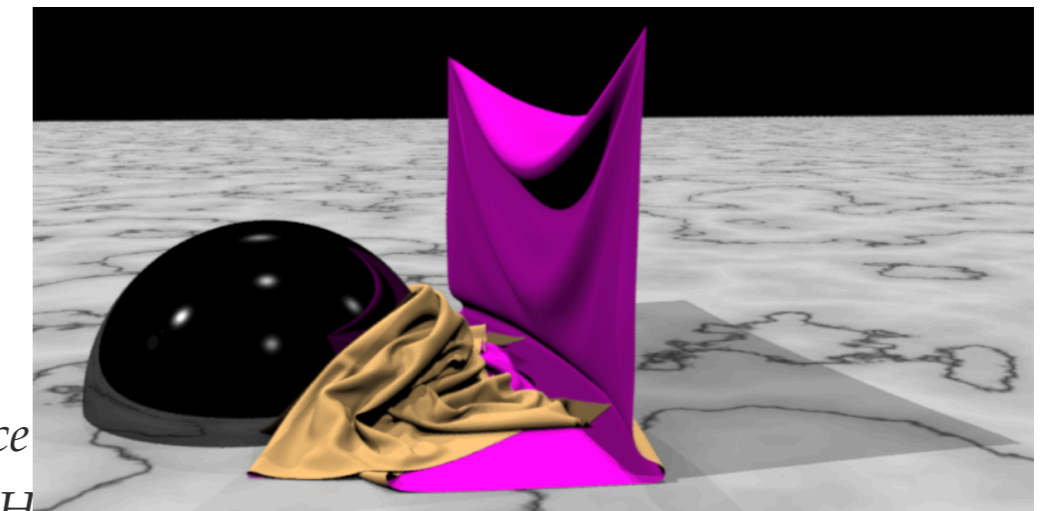
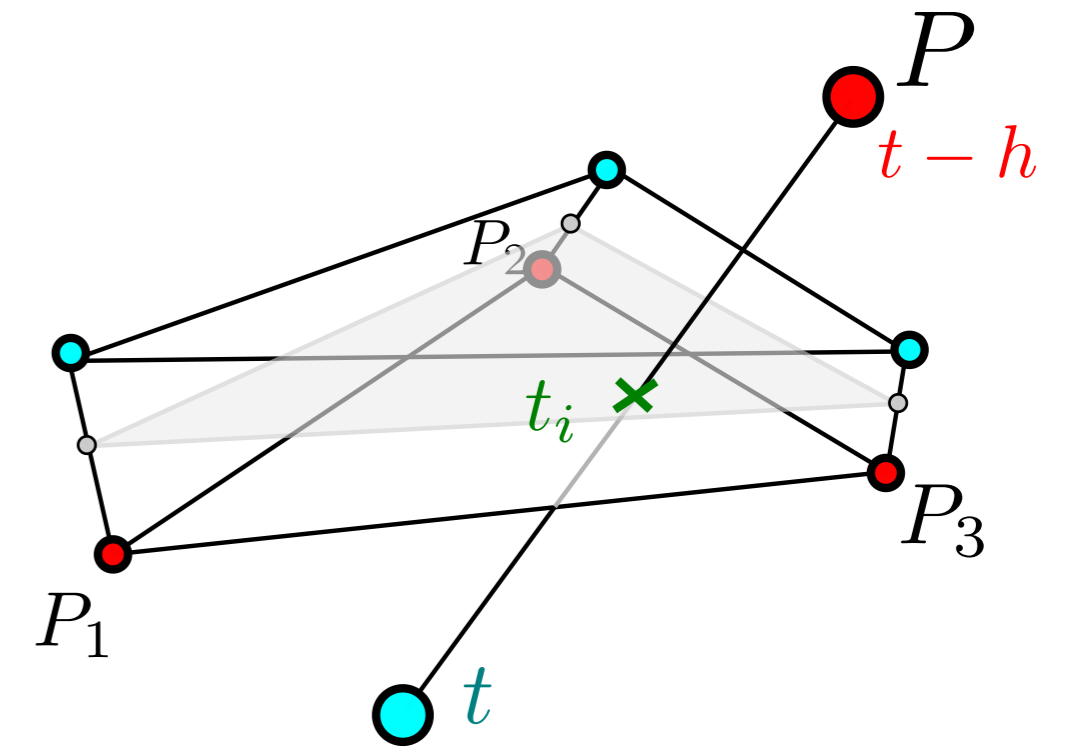
Computing intersection

Necessary condition

- Find $t_i \in [0, h]$ such that $P(t_i)$ is in triangle plane
 $(P(t_i) - P_1(t_i)) \times n(t_i) = 0$
 $n(t_i)$: normal of the triangle at time t_i

Sufficient condition

- Check $P(t_i)$ is inside the triangle
 $P(t_i) = \alpha P_1(t_i) + \beta P_2(t_i) + \gamma P_3(t_i)$
 $(\alpha, \beta, \gamma) \in [0, 1]^3, \alpha + \beta + \gamma = 1$



[X. Provat. Collision and self-collision handling in cloth model dedicated to design garments. Graphics Interface

[R. Bridson et al. Robust Treatment of Collisions, Contact and Friction for Cloth Animation. ACM SIGGRAPH 2002]

Limitation of mass spring model and continuous model

- Does mass-spring system converge toward a unique solution when sampling increase ?

⇒ No :(

Depends on the connectivity → bad for physical accuracy

Corollary

- Mass-springs work well for grid-mesh structure (draping)
- Less for arbitrary triangular meshes

1st improvment: Change toward energy formulation for bending springs (limits locking effect)

$$F = \frac{\partial E}{\partial p}$$

$$E = \frac{1}{2} K L \kappa^2, \kappa: \text{curvature}$$

[Cho et al, Stable but Responsive Cloth, ACM SIGGRAPH 2002]



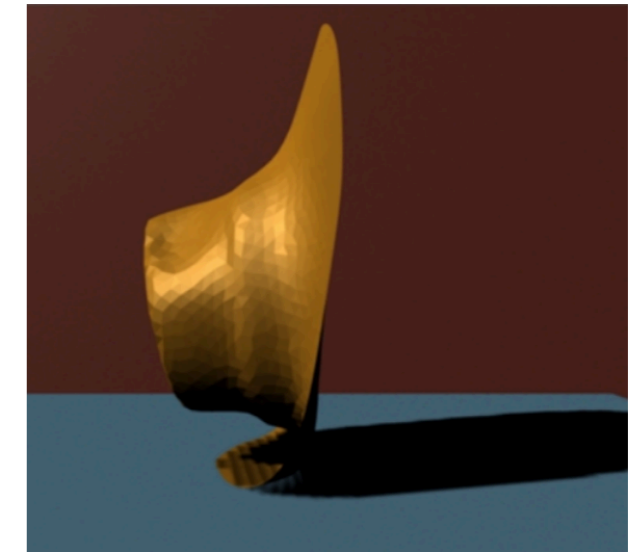
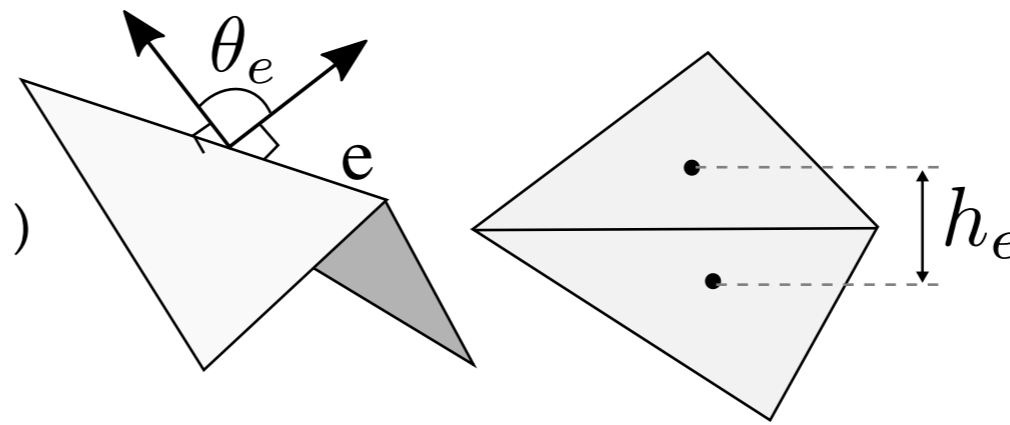
Triangle as continuous elements

- Defining Bending Energy between triangles

$$- W_B(x) = \sum_{\text{edges } e} (\theta_e - \theta_e^0) \frac{\|e^0\|}{h_e^0}$$

[E. Grinspun et al., *Discrete Shells*, SCA 2003]

(or expressed using forces in [R. Bridson et al., *SCA 2003*])



- Going toward full FEM numerical resolution

- B. Thomaszewski et al. [SCA 2006], [VRIPHYS 2008], [EG 2009].

